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QRA of hydrogen trains in rail tunnels

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Case study Rail tunnel : Severn (UK)

- L=7.012 km
- Double bore, 2 tracks
- Horse cross section: W=7.9 m, H=6.1 m





References: *M. Lipscomb, Northern Trains Ltd., Private communication, 2021.* <u>https://en.wikipedia.org/wiki/Severn_Tunnel</u> <u>https://www.networkrailmediacentre.co.uk/news/the-130-year-old-severn-tunnel-to-close-for-six-weeks-for-essential-railway-upgrade</u>

Case study Rail tunnel: Severn (UK)

- The annual average daily traffic (AADT) is 350 trains per day for each traffic direction
- train length three cars
- 64 m long
- passenger occupancy is around 148 passengers per train
- at peak times the maximum passenger load is 304 passengers

References: M. Lipscomb, Northern Trains Ltd., Private communication, 2021.



Case study Rail tunnel scenario

Assumptions:

- Tank V=160 L NWP=35 MPa
- 1 tank explodes
- FCEV is located 50 m from the tunnel entrance





References: *M. Lipscomb, Northern Trains Ltd., Private communication, 2021. S. Ring, Alstom, Private communication, 2021.*

Initiating Event								
Tunnel accident per million vehicle km	Does the accident cause a fire post crash?	Is H2 released from the system?	Is the fire extinguish ed on time?	Is H2 released from the TPRD?	Does the H2 ignite?	Does the H2 ignition is delayed ?	Event chain	Consequences
							Α	No H2 is released
		no H2 released						
	no fire						B	H2 is released but is not ignited
					no			
					ignition			
		H2 released					•	1-4 C
						immediate	C	Jet fire
					ignition		D	Deflagration of turbulent jet and possik deflagration of cloud under the ceiling
						delayed		
Creah in turnel								
Grash in tunner								
							Е	No H2 is released
			yes					
		no H2 released					F	Catastrophic rupture of the H2 tank->b wave, fireball and projectiles
				TRPD failure to open				
			no					
							G	H2 is released but is not ignited
					no ignition			
				TRPD				1-4 6
				activation		immediate	н	Jet tire
					ignition			Deflagration of turbulent jet and possil
	fire					delayed		deflagration of cloud under the ceiling
						uelayeu	j	Jet fire
						immediate		
		H2 released			ignition			Deflagration of turbulent jet and possil
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Event tree



Probability analysis

Statics for railway tunnels from International Union of Railways (UIC)

- In 2020 an average accident rate of 0.62 per million train-km is reported for a total number of 6122 per million train-km, but only 0.4% of the accident occurred in tunnels, hence a tunnel accident rate of 2.5×10⁻³ per million train-km is calculated.
- The probability that an accident in tunnels results in a **fire** is **7%**, i.e. 1 fire in 14 incidents in tunnels (UIC, 2021).

ALL RAILWAYS
Number of significant accidents
Significant accidents per million. train-km
Number of accidents with victims
Accidents with victims per million train-km
Number of victims
victims per million train-km
Number of fatalities
Fatalities per million train-km
Number of million train- kilometres



Initiating Event										
Tunnel accident per million vehicle km	Does the accident cause a fire post crash?	Is H2 released from the system?	Is the fire estinguished on time?	Is H2 released from the TPRD?	Does the H2 ignite?	Does the H2 ignition is delayed ?	Branch Frequency (per million vehicle km)	Event chain	Consequences	UK I Tuni "Sev Frec (per
/ent	tre	ρ								
		0.9	-1				2.08E-03	Α	No H2 is released	3.
	0.000									
	0.930				0.853		1 97 F- 04	в	H2 is released but is not ignited	3
					no ianition			-		
					5					
		0.1								
		H2 released				0.667	2.26E-05	C	Jet fire	4.
					0.147	Immediate				
					ignition	0 222	1 125 05		deflagration of turbulent jet and possible deflagration of cloud under	
0.0025						delaved	1.13E-05	U		2.0
Crash in						dolayou				
tunnel										
			0.00				0.005.00	=	No HQ is released	0.0
			0.00	20			0.002+00	-		0.0
		0.9	yes	10						
		no H2 released		0.030			4.69E-06	F	Catastrophic rupture of the H2 tank	8.3
			1.00	TRPD failure to open						
			no		0.800		1.21E-04	G	H2 is released but is not ignited	2.
				0.970	no ignition			-		
				TRPD						
				activation		0.667	2.02E-05	н	Jet fire	3.6
					0.200	immediate				
	0.070	\sum			ignition				jet deflagration and/or flammable cloud deflagration under the ceiling (if	
	fire					0.333	1.01E-05		created) and DDT	1.8
	nre					0 elayed	1 16E-05		.let fire	20
					1	immediate	1.102-05	1		2.1
		0.1			•					
U, I		H2 released			ignition	0.333	5.78E-06	к	deflagration of turbulent jet and possible deflagration of cloud under the ceiling	1.0
<i>7 7 7</i> 7						delaved				

Probability analysis

Probability of H₂ release post-crash

P =0.10

- Scarce published crash test data on H₂ vehicles: 5 tests.
- In all 5 tests there was not enough damage to the system for it to leak or release hydrogen.
- Sandia used a gamma distribution conjugate (Jeffreys) prior to account for a half of an event (0.5).
- 10% probability of a release



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Sandia Report - Sand2017-11157

Figure 6. Uncertainty distribution on the probability that a crash results in hydrogen release.

Probability of TPRD failure Localised fire



- Failure rate of TPRD statistics are not available.
- Sandia suggested a value for TPRD failure probability (0.03) obtained as average of the beta distribution (0.5, 16.5)

Table 2 Summary of TPRD Operations in Hydrogen Tank Fire Experiments [20-24]

Source	TPRD demands	TPRD operation		
Yamazaki	2	2		
Suzuki	4	4		
Zheng	1	1		
Wyandt	6	6		
Sekine	3	3		

Assuming a Jeffrey's beta prior distribution, the data in Table 2 results in a Beta(0.5, 16.5) distribution





B.D. Ehrhart, D. M. Brooks, A. B. Muna and C. B. LaFleur Fire Technology 2019 https://doi.org/10.1007/s10694-019-00910-z

Figure 8. Uncertainty distribution on the probability that a TPRD will fail to operate on demand.

Probability analysis Probability of H₂ ignition

TPRD	Initial mass flow rates (kg/s), for:						
(mm)	Car (700 bar tank)	Bus/train (350 bar tank)					
0.5	0.0067	0.0038					
1	0.0268	0.0150					
2	0.1072	0.0601					
3	0.2412	0.1353					
4	0.4289	0.2405					
5	0.6701	0.3757 Bus/ t					
6	0.9649	0.5410					

P = 0.08 for car P=0.2 for bus/train





Probability analysis

Probability of immediate ignition

P = 0.667

• The probability of an **immediate ignition** (given that an ignition will occur) is 66.67%, and the complimentary probability of delayed ignition is 33.33%.

Hydrogen Release Rate (kg/s)	Immediate Ignition Probability	Delayed Ignition Probability
<0.125	0.008	0.004
0.125 - 6.25	0.053	0.027
>6.25	0.23	0.12
Average	0.098	0.049

Table 2: Hydrogen ignition probabilities.

Sandia Report - Sand2017-11157



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/ent	tro	Δ								
		0.9					2.08E-03	Α	No H2 is released	3.71
	0.000	no H2 released								
	0.930				0.853		1 97E-04	B	H2 is released but is not ignited	3.50
					no ignition		1.57 E-04		The released but is not ignited	0.02
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		0.1						_		
		H2 released				0.667	2.26E-05	С	Jet fire	4.04
		\sim			0 147	Immediate				
					ignition	0.333	1 13F-05	п	deflagration of turbulent jet and possible deflagration of cloud under the ceiling	2.02
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Crash in tunnel										
			0.00)			0.00E+00	E	No H2 is released	0.00
		0.9	yes	no						
		no H2 released		0.030	>		4.69E-06	F	Catastrophic rupture of the H2 tank	8.38
			1.00	open						
			no	0.970	0.800	\geq	1.21E-04	G	H2 is released but is not ignited	2.17
				TRPD activation		0.667	2.02E-05	н	Jet fire	3.62
	0.070	5			0.200 ignition	Immediate			jet deflagration and/or flammable	_
		\square				0.333	1.01E-05	I.	cloud deflagration under the ceiling (if created) and DDT	1.81
	fire					delayed				
		01			1	0.667 immediate	1.16E-05	j	Jet fire	2.07
UN	Je	H2 released			ignition	0.333	5 . 78E-06	к	deflagration of turbulent jet and possible deflagration of cloud under the ceiling	1.0
7 <i>4</i> 7						delayed			·•	

Example of Railway tunnel



 Calculations of flame lengths and three hazard distances for free hydrogen jet fires, ("E-Laboratory"; Molkov, 2012)



Consequence analysis Blast wave decay in a tunnel

• Universal correlation for the blast wave decay after a hydrogen tank rupture in a tunnel fire (Molkov and Dery, 2020). $\Delta P = P0 * \overline{P} = P0 * 0.22 * \left(\frac{P0 LP}{4 E A P0.5} * f L\right)^{-0.35}$



Example of Railway tunnel Blast wave decay



Tank rupture near the end of the 7 km road tunnel: blast waves after rupture of 160 L tanks with different SoCs



Overpressure Hazard Probit function for harm to people and structural damage



Fig. 2 – Comparison of overpressure probit functions for harm to people.

Fig. 4 - Comparison of structural damage probit functions.

La Chance et al. International journal of hydrogen energy 36 (2011) 2381-2388



Example of Railway tunnel Percentage of Fatality and Damage



Probability of Fatality < 1% at 200 m

Probability of damage = 20% at tunnel entrance Probability of damge < 1% at 900 m



Example of Railway tunnel

Individual risk

IR = Frequency of tank Rupture (per year) x Probability of Fatality



• passenger occupancy :148 passengers per train

Consequence analysis DDT potential (KIT)

- A tool for the assessment of a detonation case is here taken into account to evaluate the consequence of the hydrogen detonation in the tunnel.
- It is assumed to be the consequence of the release of hydrogen from TPRD, when TPRD is activated by a fire, and a strong ignition at the top of the tunnel at an unfavourable time and location.
- The pressure loads are calculated to evaluate the consequence of the hazard.



Example of Railway tunnel DDT potential

Case (I):

- $\hfill\square$ Single rail tunnel of two-tubes tunnel with a circular cross-section 64.3 m^2
- □ Equivalent diameter Deq=8.98 m
- \Box Tunnel roughness equivalent to BR = 1% which is equal to 2.2 cm of roughness.
- □ Hydrogen inventory 5.8 kg due to the accident, then cloud formation with a late ignition.

Uniform hydrogen-air mixture of 10 to 30% H₂ in air filled a layer of h=0.6 m thick above the train. The cloud is formed in a gap between the roof of the train and the ceiling

Case (II):

- □ Single rail tunnel of two-tubes tunnel with a circular cross-section 64.3 m²
- □ Equivalent diameter Deq=8.98 m
- \Box Tunnel blockage by the train is equivalent to BR = 40%.
- \square Hydrogen inventory 5.8 kg due to the accident, then cloud formation with a late ignition.
- □ Stratified hydrogen-air mixture filled the whole tunnel cross-section

A linear hydrogen concentration gradient with maximum concentration 10, 15, 20, 25, 30% H_2 at the ceiling and 0% H_2 at the bottom of the tunnel is assumed

Uniform H₂-air mix

Stratified H₂-air mix



Figure 1. Hydrogen cloud geometry: a layer of uniform hydrogen-air mixture (a); fully filled tunnel cross- section with a stratified hydrogen-air mixture (b).



Example of Railway tunnel DDT potential

Initial hydrogen inventory, mass flow rate and discharge time for train

Vehicle	Total Vehicle Inventory (kg)	Single Tank Inventory (kg)	Initial mass flow rate (kg/s)	Discharge time (sec)	Cross- section area (m ²)	
Train 1 (350 bar)	96.0	4.14	7.85	67	10.7	
Train 2 (350 bar)	105.0	5.80	5.89	97	13.9	



Example of Railway tunnel

Results of Flame propagation and DDT

- Independent of hydrogen inventory, for maximum hydrogen concentration of 10 and 11% H₂ the flame cannot accelerate to the speed of sound. It will propagate as a slow subsonic flame with a maximum combustion over-pressure 1-2 bar.
- Independent of maximum hydrogen concentration at the ceiling, for hydrogen inventories 5.8 and 10 kg the only slow subsonic flame with a maximum combustion over-pressure 1-2 bar may develop because too small size of the cloud.
- Only in the case IV for 100 kg of hydrogen inventory the size of the cloud will be enough for flame acceleration and detonation onset at maximum hydrogen concentration above 15%. Then, it needs the ventilation to keep hydrogen concentration below 15% to prevent the detonation.



Conclusions

- The results of the frequency analysis showed that the most likely consequence includes scenarios with no release of hydrogen or hydrogen release without ignition.
- When the hydrogen does ignite, it is most likely a jet fire from the hydrogen system or a TPRD.
- In the presence of a localised fire, if the TPRD fails to open, the catastrophic H₂ tank rupture is the most likely scenario.
- The risks with the largest consequences are shown to be scenarios leading to hydrogen flammable mixture deflagration (could be eliminated by proper TPRD design) and tank rupture in a fire (could be eliminated by using innovative explosion free in a fire tanks, i.e. micro LNB safety technology).





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This project has received funding from the Fuel Cells and Hydrogen 2 Joint Undertaking (now Clean Hydrogen Partnership) under Grant Agreement No 826193. This Joint Undertaking receives support from the European Union's Horizon 2020 Research and Innovation program, Hydrogen Europe and Hydrogen Europe Research.

Clean Hydrogen Partnership



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